# 3.10.002 ADVANCES IN HIGH EFFICIENCY COUPLING TO HEAVY ION DIRECT DRIVE AND APPLICATION TOWARDS SMALL TEST REACTORS

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Michael Hay (UC Berkeley)
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Driver energy (MJ)

Yield (MJ) / Gair

 $\eta_{absorbed}$  /  $\eta$ 

Peak drive power (TW)

In-flight aspect ratio

Convergence ratio

In-flight adiabat  $\alpha$ 

0.36

195

2.4

24.7 / 77

0.97 / 0.10

21.6 / 60

0.91 / 0.10

0.44

205

3.2

20.8 / 47

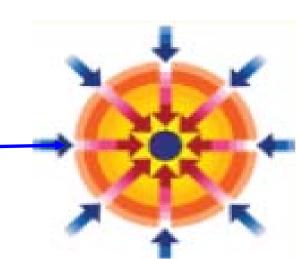
0.88 / .09

1.3

0.16 / 0.02

1.4

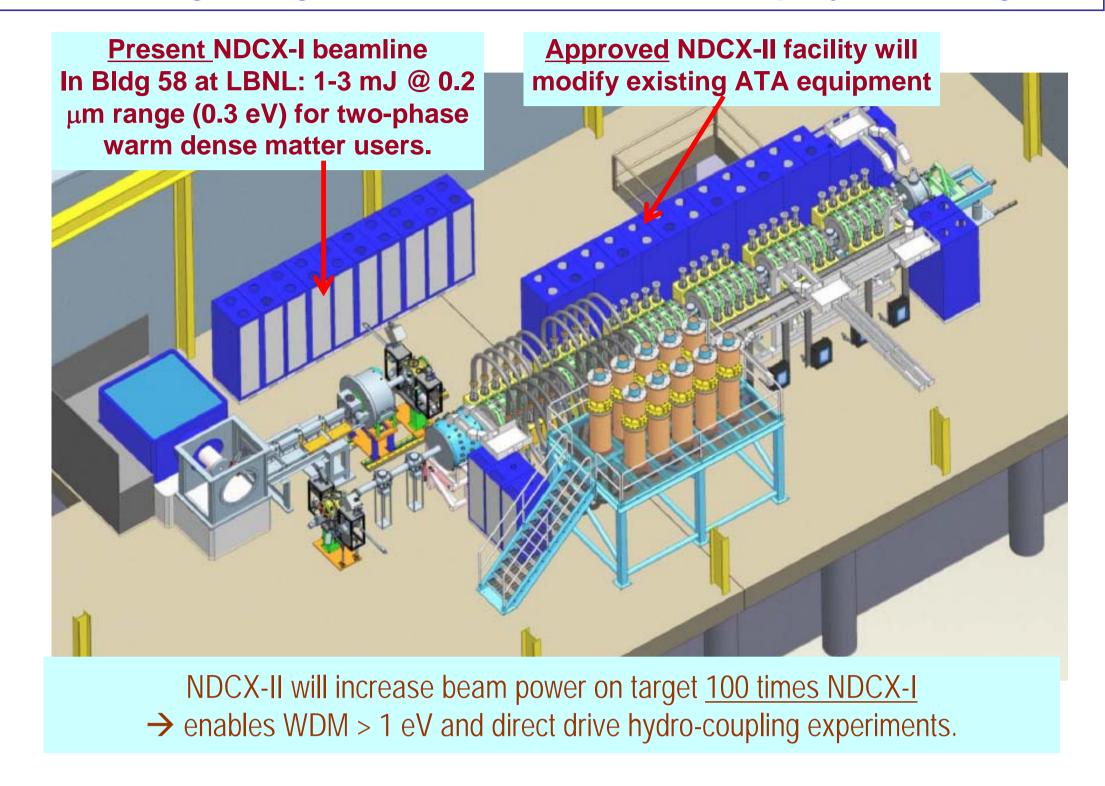
...exploiting the intrinsic high overall drive efficiency of heavy ion beams for direct drive \_



6<sup>th</sup> International Conference Inertial Fusion Science and Applications, San Francisco, California, Sept. 6 -11, 2009

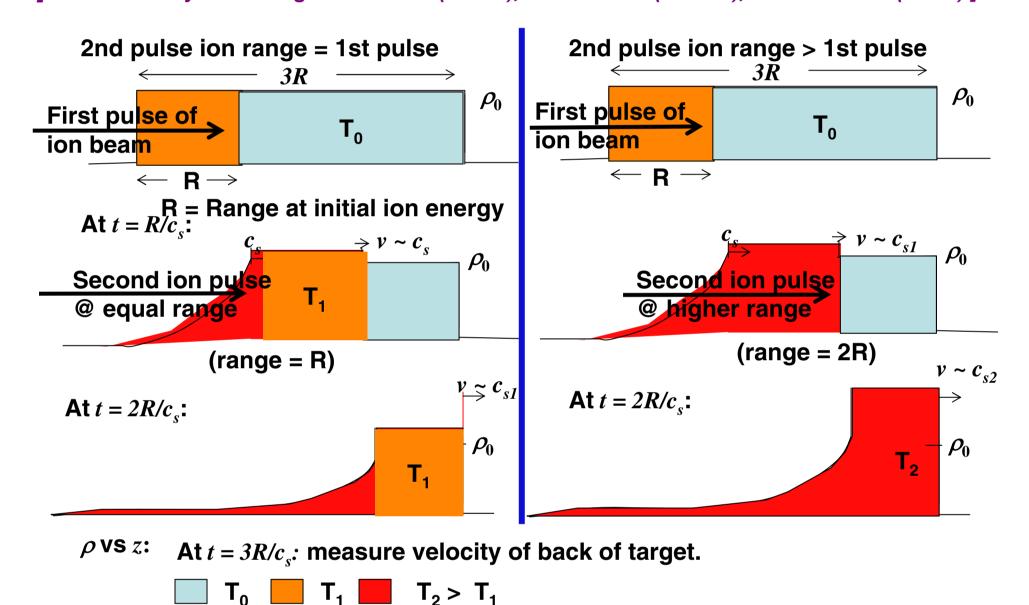
#### Recent innovations, together with NIF ignition, would support →a new vision for heavy ion fusion: Optimizations of direct drive using HYDRA Heavy ion beam intensity increases > 1000X with velocity increasing in time with space charge neutralized by background plasma. [Neutralized Drift --in progress (Michael Hay) Compression Experiment (NDCX): P. K. Roy, et. al. Phys. Rev. Lett. 95, 234801 (2005), and J.E. Coleman et al., in Proc. of the 2007 Particle Accelerator Conf., •Simulations conducted with HYDRA [2], a •Pure-DT targets are easily fabricated Albuquerque, NM, 2007(IEEE catalog# 07CH37866, USA, 2007). Time-dependent fully 3-D radiation hydrodynamics code •RT-robust: Atwood number = 0, no inchromatic focusing correction experiment planned in NDCX next year]. developed at LLNL flight mixing of fuel and ablator material 2. High hydro-drive efficiency of heavy ion beam direct drive in ablative rocket •HYDRA employs arbitrary Lagrangian •Total fuel mass = 1.344 mg; payload mass regime (also uses beam velocity increasing in time-focus of this poster). Eulerian hydrodynamics and a monotonic fraction = 1/3, corresponding to a rocket [B. G. Logan, L. J. Perkins, and J. J. Barnard, Phys. Plasmas 15, 072701 (2008)]. artificial viscosity model to resolve shock efficiency of 60% 3. Beam spot rotation on target with helical RF-beam perturbations upstream [B. fronts Sharkov (Russia), S. Kawata (Japan), H. Qin (USA)] -> enables direct drive with Our implosion calculations utilize many of <-- DT ablator (0.2564 g/cc) only 4 polar angles @< 1% non-uniformity for direct drive [J. Runge, Germany]. HYDRA's multiphysics capabilities e.g. 3-D 0.8695 mm <-- DT fuel (0.2564 g/cc) raytrace, heavy ion deposition, flux-limited 4. New agile on/off valve technology for liquid jets adapted to provide thick liquid 0.7011 mm multigroup radiation diffusion, quotidian protection for direct drive chambers. [R. Moir, LLNL, 1999 HYLIFE note and equations of state, and multigroup charged recent advances-see http://videos.komando.com/2008/08/19/water-painting/]. $\leftarrow$ DT gas (2.e-4 g/cc) particle transport (1) Breakthrough: Compression of velocity-chirped ion beams in plasma ((Roy et al PRL 95(2005) 23481) Now, radial and temporal compression $\rightarrow$ 2000 X $n_{beam}$ •No zooming – a substantial portion of the [2] M. M. Marinak, et al. Phys. Plasmas 8, drive goes unabsorbed 2275 (2001). -Experimental •Ion energy ramped from 50 to 500 MeV in a single jump as in Ref. 1 base case Lagrangian r-t plot follows location of each zone/mass element through implosion •Minimal (passive) range lengthening at constant 50 MeV Rb ion energy through 14 ns /elocity tilt Time (µs) **←500 MeV Recent Hydra results** 200 A smaller focused spot size at peak current with combined axial and radial bunch compression in a denser plasma background Rb ion beam kinetic 40 Pulse compressed energy ~2 ns FWHM 100 (2) Following our success in velocitychirp compression of intense ion beams **←50 MeV** to few-nanosecond pulses in plasmas... - we have another powerful fusion idea which also uses ion velocities increasing in time: Time [ns] Strongly-increasing >4X ion range **Constant ion range** → high hydro-coupling efficiency! → decouples Heavy-ion direct drive LASNEX runs (June 2007) by John Perkins (LLNL) found high target gains $\geq$ 50 at 1MJ with low range ions @ high drive hydro coupling efficiency (16%) (Phys. of Plasmas 15, 072701 2008) Heavy-ion direct drive (1MJ) . CH shell 1.0MJ ablator cr 1 .9mm 0.025 · Rb ion range → DT gas Time (ns) —Preheat problem-avoidable w/ small C doping ≥ 0.015 All DT ablator ablator All DT DT/CH ablator 0.005 0.0055 0.006 0.0065 0.007 Ablator rho-R (g.cm-2) Ablator rho-R (g.cm-2) NIF ignition would validate key requirements for adequate gain HIF achievable in NIF-similar-scale fuel capsules using direct drive @ 300-500 kJ driver energy. John Perkins, February 2009) Time [ns] *Ion energy and range increase during the drive* • Yield = 39.8 MJ / Gain = 90.4→ increases hydro coupling efficiency • Absorbed energy fraction = 0.92 HI beam DT fuel Low aspect ratio and Atwood •Coupling efficiency = 0.099 **↑** Time number at fuel-ablator interface--gas • Hydrodynamic efficiency = 0.087 expect robust RT stability AR(0)=2 (to scale) (2-D RT calculations in progress) •IFAR = 27.5, convergence ratio = 29.5, adiabat = 2.723.0 $m_{ablator}/m_{fuel}$ 18

Construction of NDCX-II began July 2009→enables higher energy warm dense matter and planar direct drive hydro-coupling research beginning 2<sup>nd</sup> half of 2012 (Joe Kwan, project manager)

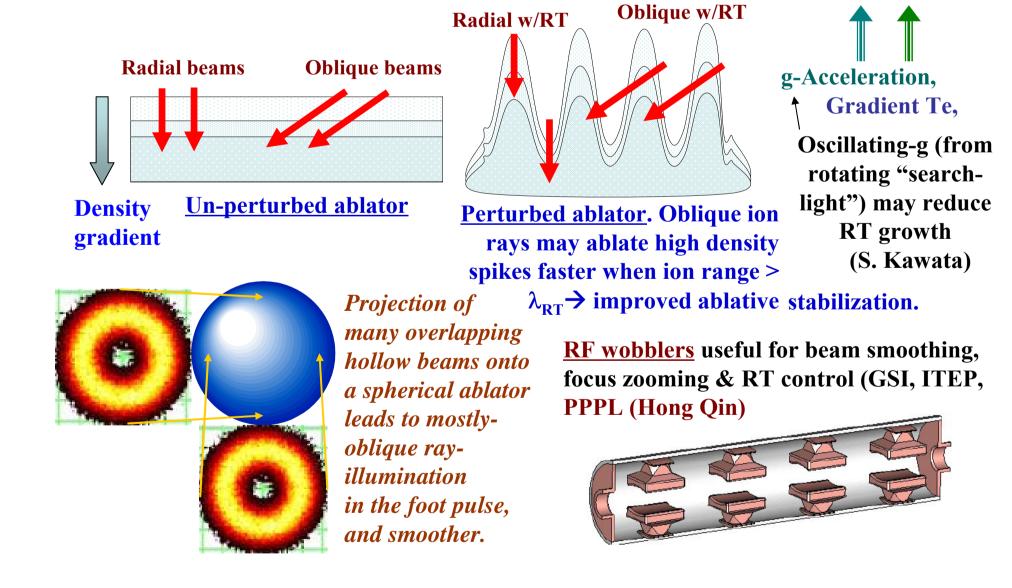


NDCX II can explore improvement in hydro-coupling efficiency with increasing ion range, either ramped or double pulse.

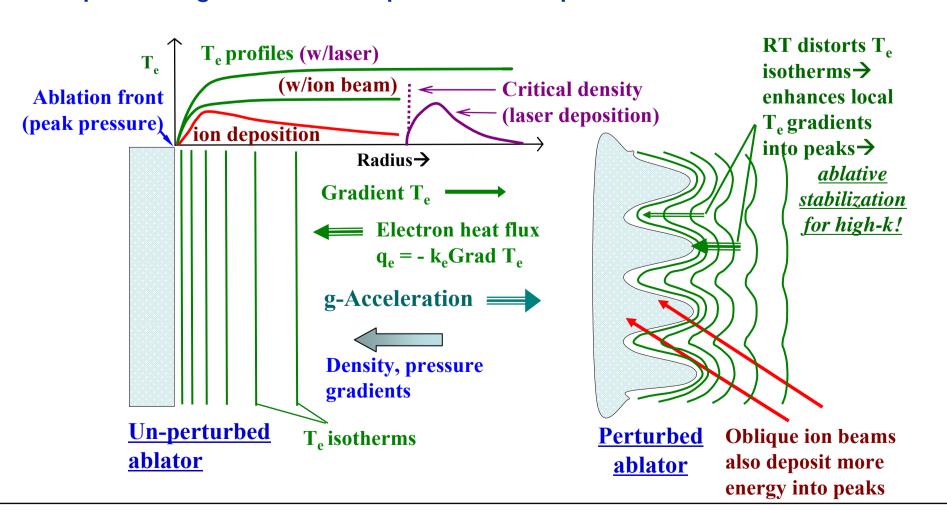
[Simulations by Siu Fai Ng & Simon Yu (CUHK), Seth Veitzer (Tech-X), John Barnard (LLNL)]



(3) Oblique ion illumination with beam spot rotation (with RF wobblers) can enhance ablative-stabilization and lengthen pressure gradient scale lengths behind the ablation front



Ablative stabilization of high-k RT modes depends on local electron temperature gradients from peak beam deposition to ablation front



Ion versus laser beams-for the same PdV work at the ablation front:

→ ion beam energy deposited closer to ablation front (higher coupling efficiency)

→ pressure gradients and Atwood numbers may be smaller with DT ablators







• Max. shell velocity =  $3.51*10^7$  cm/s

## (SUB-MJ DRIVE FUSION AND FUSION-FISSION HYBRIDS)\*

NIF ignition should renew interest not only in laser IFE, but also in Heavy Ion Fusion, for reasons that still apply today:

- MJ-beam accelerators have separately exhibited intrinsic efficiencies, pulse-rates, average power levels, and durability required for IFE.
- Thick-liquid protected target chambers are designed to have 30 year plant lifetimes.
- Focusing magnets for ion beams avoid direct line-of-sight damage from target debris, n and g radiation.
- Heavy ion power plant studies have shown attractive economics and environmental characteristics (only class-C low level waste). [Yu et al., Fusion Sci. Tech. 44, 2 (2003) 329]

#### Copies of these IFE reviews available upon request

1979 Foster Committee

1983 Jason Report (JSR82-302)

1986 National Academies of Sciences Report

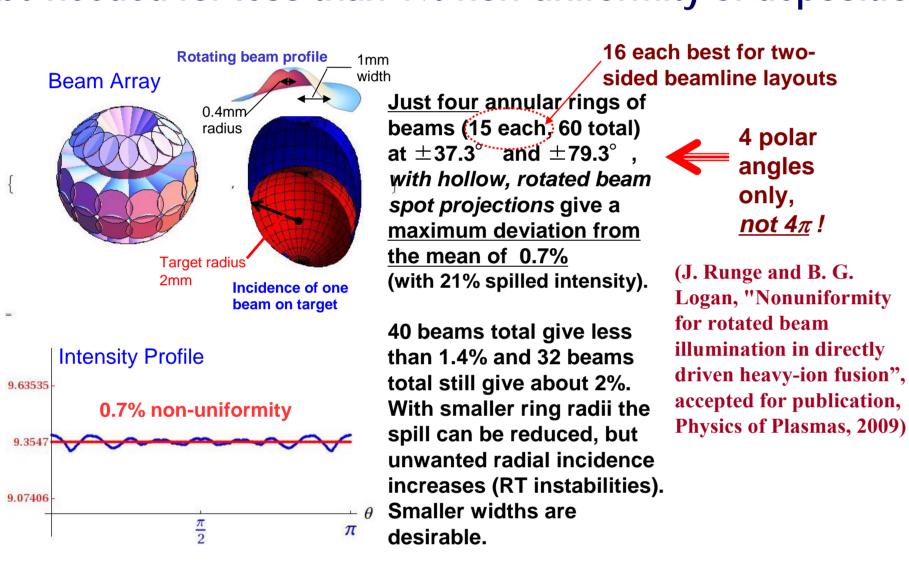
1990 Fusion Policy Advisory Committee report (Stever Panel) 1993 Fusion Energy Advisory Committee (Davidson Panel)

1996 FESAC report (Sheffield Panel)

Applications of heavy ion direct drive for fusion and fusion-fission hybrids requires R&D on targets, chambers, and accelerator drivers that can work together. .

#### (3) Illumination Geometry:

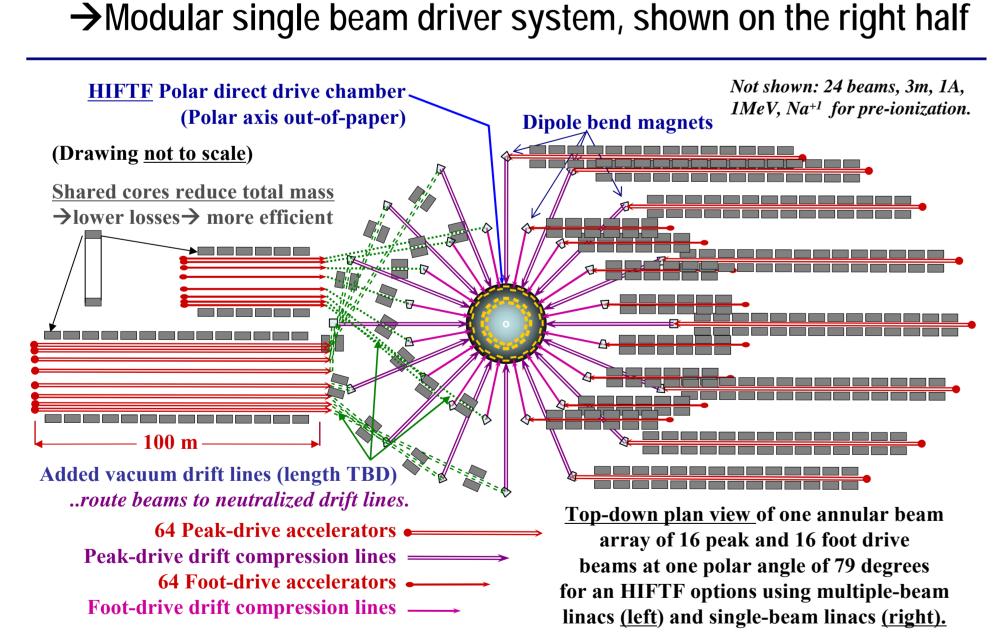
Jakob Runge, (Fulbright summer student 2008 in LBNL), developed a Mathematica model to explore the question: what minimum number of polar angles of annular ring arrays with beams *using hollow rotated beam spots* are be needed for less than 1% non-uniformity of deposition?



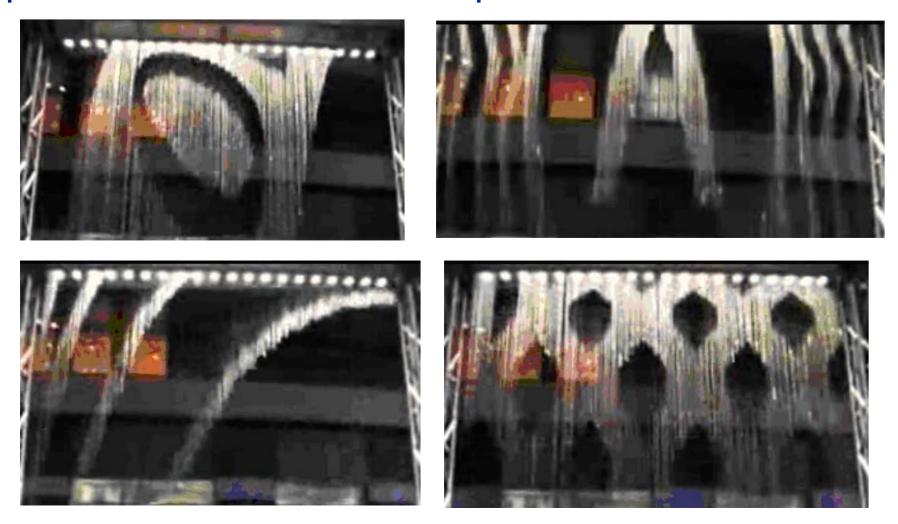
Induction linear accelerator design for heavy ion direct drive w/ four-ring polar angle target illumination: future studies can consider modular, single beam driver option if target gains > 100, otherwise, we can consider the option to use multiple-beam induction linacs (more efficient with shared cores)-both options are depicted below:

Top down plan view of two types of beam layout options:

→ Multiple-beam linac option shown on the left half of beams



(4) New <u>pulsed-jet</u> valve capability would enable thick liquid Flibe protection like HYLIFE to be adapted to *direct drive chambers* 



[R. Moir, LLNL, 1999 HYLIFE note. Water fountain pictures from http://videos.komando.com/2008/08/19/water-painting/].

For R&D planning, its time to re-examine issues and needed facilities for <u>all</u> driver, target and chamber options. (Example tables below may be incomplete).

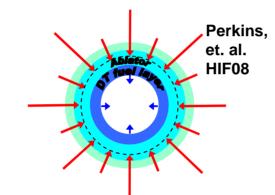
#### Example HIF driver options, some associated key issues & R&D facilities

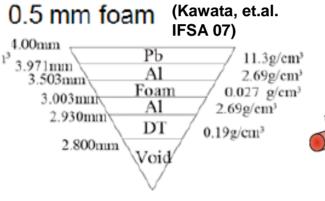
HIF Driver Options	Multi-beam LIA- magnetic quadrupole	Multi-beam LIA magnetic solenoids	Multi-beam LIA- electric quadrupoles	Modular set single-beam LIA-solenoids	Induction Synchrotron, RF linacs
Key Issues	SC magnet cost and multi-beam E-cloud issue	SC magnet cost & multi- solenoid field asymmetries	Limited λ <sub>b</sub> & longitudinal compression under accel.	Efficiency>0.2 requires high $\lambda_b$ >100 $\mu$ C/m >2 kA/beam!	Viable only for 100 GeV targets? # of beams > 1?
R&D Facilities -up to non- ignition scale implosions	Modified HCX + 10 kJ IRE scale linac for direct drive exp. or MJ-scale for indirect drive	Modified HCX + 10 kJ IRE scale linac for direct drive exp. or MJ scale for indirect drive	Modified HCX + 10 kJ IRE scale linac for direct drive or MJ scale for indirect drive	NDCX-II experiments using higher q/A ions + 10 kJ IRE scale linac for direct drive	KEK-AIA?  10 kJ scale accelerator tests, then MJ scale for implosion test

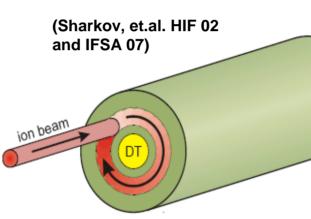
#### Example HIF target options, some associated key issues & R&D facilities.

Example file target options, some associated key issues & R&D facilities					
HIF Target Options	Indirect-Drive Hohlraum, cylindrical, two sided illumination	Direct-drive, ablative, multi- polar angle ring illumination	Direct/Indirect "Cannonballs" (Spherical hohlraums)	Direct-drive Cylindrical (ITEP-TWAC)-Fast Ignition	
Key Issues	Low ~<2% coupling efficiency→7 to 8 MJ (RPD)	High contrast pulse shape, beam balance, # beams need	Case losses, minimum Tr for radiation coupling test	Cost of 100 GeV, 10 MJ beams, beam spot rotation	
R&D facilities (non-ignition scale)	1 GeV, > 1 MJ, >60 beams,~ 0.5 mm spots for hohlraum implosion test	HIDDIX (IRE~ 100 MeV, 10 kJ scale, 60+? beams for cryo implosion test	~> 1 GeV, > 1 MJ, spot size < 1 mm, > 60? beams for implosion test	TWAC, KEK-AIA? Beam requirements for implosion test?	



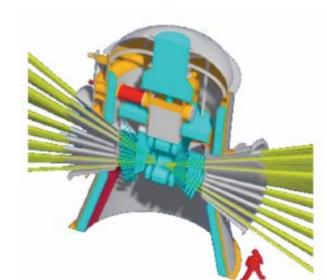


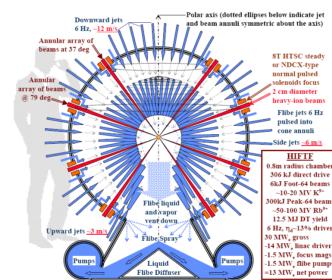


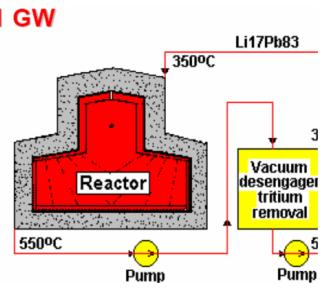


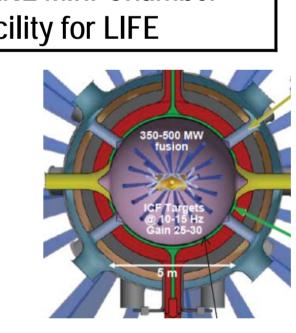
#### Example HIF chamber options, some associated key issues & R&D facilities.

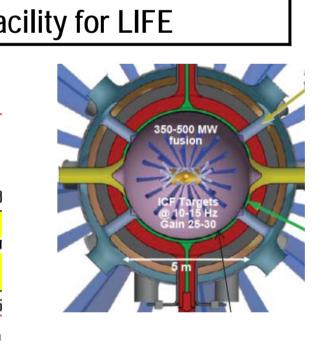
Example file chamber options, some associated key issues a Rab facilities					
HIF Chamber Options	Thick liquid chambers- oscillating jets (HYLIFE)	Pulsed radial liquid jets, polar geometry (TOFE 08)	Thin liquid metal surface- protected chambers (ITEP)	Solid wall, gas protected Dry wall (LIFE)	
Key Issues	Pumping power, oscillating nozzles, pulse rates < 6 Hz	Pumping power, precision jet control for polar beam ring access	Recovery rate for re- wetting walls. Neutron damage to structures.	Cryo targets in 6000K hot gas, solid wall metal dust blowout	
R&D facilities (non-ignition scale)	1 M \$ scale exp. followed by 10 M\$ scale hydro-equiv water simulator tests	1 M \$ scale exp. followed by 10 M\$ scale hydro- equiv water simulator tests	1 M \$ scale exp. followed by 10 M\$ scale hydro- equiv Hg or NaK metal film recovery test	Collaborative experiments in planned LLNL Mini-Chamber facility for LIFE	











Concept for Advanced T-Lean (Mostly DD) HIF power plant to produce plasma for MHD direct conversion

vent down

Flibe Spray

Heavy ion fusion direct drive might

heavy ion

fusion

hybrid

Fusion gain G<sub>NIF</sub> for laser

hohlraums (like NIF) and for

generic advanced IFE gain Gady

(such as heavy ion direct drive

versus driver energy Ed (MJ).

Fusion yield =  $20 \times 0.25 \text{ MJ} = 5 \text{ MJ}$ .

Low pulse repetition rate = 2 Hz

Average fusion power = 10 MW

Blanket fission power density = 1 MW/m<sup>3</sup>

Polar axis (dotted ellipses

below indicate jet and beam

annuli symmetric about the

**8T HTSC** 

or NDCX-type

normal pulsed

2 cm diameter

Flibe jets 6 Hz

pulsed into

Side jets

<u>~6 m/s</u>

heavy-ion

η<sub>d</sub>G<sub>adv</sub>=2, @ η<sub>d</sub>=0.1

P<sub>edriver</sub>= 5 MW<sub>e</sub>

 $P_{enet} = 33 MW_{e}$ 

Downward jets 6

Hz,  $\sim 12 \text{ m/s}$ 

Upward jets ~3 m/s

Annular array of

beams at 37 deg

Fission power = 80 MW

Chamber radius = 1.2 m

Wall loading = 0.3 MW/m<sup>2</sup>

Uranium fuel mass = 1.3 tons

Concept for thick-liquid-protected

HIFTF chamber for polar direct drive

→Small HIF hybrid example

is given below

lead to a much smaller hybrid

 $G_{NIF}(E_d)$ 

 $G_{adv}(E_d)$ 

condenser Liquid jets (3.4 Hz annular cones that merge into liquid e.g. Flibe or Li beams at 37 deg Upward jets ~3 m/s

→ Peter Seidl will be organizing HIF "Renew" workshops (soon-dates TBD)

- Pulsed jets (Moir: 1999 HYLIFE notes) merge radially halfway into chamber, forming a 30-cm thick <u>liquid imploding shell</u> with annular beam access around the axis at shot time, @ 4 angles.
- Liquid shell mass and momentum sufficient that pocket pressurization due to non-neutron fusion yield slows but does not reverse the liquid radial velocities of all but the slowest upward jets.
- •Jet velocities decrease with polar angle for net momentum of the liquid and post-shot vapor to vent downwards to clear the chamber.

**HIFTF** 0.8m radius chamber 306 kJ direct drive 6kJ Foot-64 beams ~10-20 MV K<sup>9+</sup> 300kJ Peak-64 beams ~50-100 MV Rb<sup>9+</sup> 12.5 MJ DT yield 6 Hz,  $\eta_d \sim 13\%$  driver 30 MW<sub>e</sub> gross -14 MW<sub>e</sub> linac driver -1.5 MW<sub>e</sub> focus mags -1.5 MW<sub>e</sub> flibe pumps =13 MW<sub>e</sub> net power

**Advanced fuel HIF Power Plant (HIFPP)** using direct drive compression of DD fuel with DT spark plug. 1.4 m radius chamber 1.6 MJ direct drive: Foot-64 beams ~20-40 MV K<sup>9+</sup> Peak-128 beams ~100-200 MV Rb<sup>9+</sup> 100 MJ DD/DT yield 1.5 Blanket energy M 3.4 Hz,  $\eta_d \sim 13\%$  driver  $_{\text{lconv}} = 0.7 [0.5 \text{ MHD} +$ 0.4 thermal bottom 357 MW<sub>e</sub> gross -42 MW<sub>e</sub> linac driver -8 MW<sub>e</sub> all magnets -7 MW<sub>e</sub> liquid pumps = 300 MW<sub>e</sub> net power

### **Conclusions:**

- → Heavy ion direct drive results so far look very encouraging.
- → Much more theory, experiments and conceptual design are needed for:
- ■2-D and 3-D symmetry and Rayleigh Taylor stability studies.
- ■Graded DT→D→ ablators for higher stopping power
- ■Ion Beam brightness, neutralization, collective effects, stripping.
- •Multiple-beam induction linacs for higher efficiency, lower cost Development of RF wobblers and time-dependent focus control for hollow-beam spots.
- Pulsed liquid jet control experiments for direct-drive chamber protection.